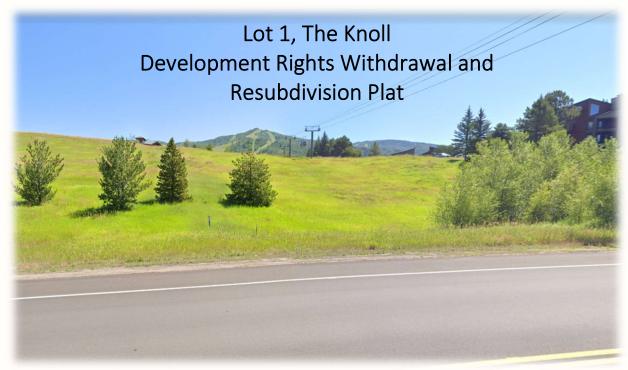


DRAFT

Drainage Study and Stormwater Quality Plan



Original Date: October 5, 2022

Prepared by: Matthew Eggen, P.E.

NOTE

City of Steamboat Springs plan review and approval is only for general conformance with City design criteria and the City code. The City is not responsible for the accuracy and adequacy of the design, dimensions, and elevations that shall be confirmed and correlated at the job site. The City of Steamboat Springs assumes no responsibility for the completeness or accuracy of this document





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APPENDIX D Ownership and Maintenance Plan (with final Drainage Study)

APPENDIX E City Forms & Checklists:

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Form 4 Stormwater Quality Plan Checklist

Project Sheet(s)

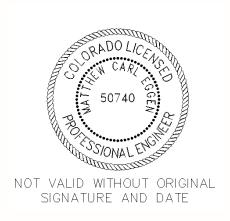
Design Checklist SWQCV Standard





CERTIFICATION

I hereby affirm that this Drainage Study and Stormwater Quality Plan for the Preliminary Plat of Lot 1, The Knoll Development Rights Withdrawal and Resubdivision Plat was prepared by me (or under my direct supervision) for the owners thereof and is, to the best of my knowledge, in accordance with the provisions of the City of Steamboat Springs Storm Drainage Criteria and approved variances. I understand that the City of Steamboat Springs does not and will not assume liability for drainage facilities designed by others.



Matthew Eggen, P.E. State of Colorado No. 50740





INTRODUCTION AND LOCATION

The purpose of this drainage study and stormwater quality plan is to develop an analysis of stormwater runoff and drainage structures required for Lot 1, The Knoll Development Rights Withdrawal and Resubdivision Plat. Included in this study are all the base data, methods, assumptions, and calculations for the stormwater management system for the development of the property. It is submitted in conjunction with the Preliminary Plat, dated October 5th, 2022.

The facts and opinions expressed in this report are based on Landmark Consultants, Inc.'s (Landmark's) understanding of the project and data gathered from:

- Site visit (summer 2022)
- Steamboat Springs GIS data
- NRCS soil maps
- FEMA FIRM Community Panel Numbers 08107-CO883-D (February 4, 2005)
- Detailed field survey by Landmark Consultants, Inc.
- Citywide Stormwater Master Plan, March 2013.
- References listed at the end of this report

The original Steamboat Grand Resort Hotel Condominium ("Hotel") Declaration and Plat located on Lot 1; The Knoll was recorded September 20, 2000. Of the original 19.96-acre Lot 1, about 13.99-acres were defined as a separate parcel that was subject to Future Development Rights, as shown on the plat recorded at file number 12907.

On July 1, 2005, the 'Second Supplement to the Condominium Map and Plat of the Steamboat Grand Resort Hotel Condominium" was recorded that showed areas that were released from Future Development Rights and defined the remaining 4.35-acre area subject to development rights. The development rights on the 4.35-acre parcel which shall be referred to as the "Development Parcel" are currently owned by Steamboat Resort Development Company, an affiliate of Alterra Mountain Company.

This preliminary plat application is submitted for the purpose of withdrawing the Development Parcel from the Hotel Condominium and subdividing such parcel in to 2 lots, one referred to in the Application as Lot 1 and the other as the Tram Lot. A small portion of the Development Property on the southernmost portion of the Hotel building consisting of the area occupied by the mechanical room and a portion of the underground parking structure, adjusted to include eaves, veneers and other features will not be withdrawn from the Hotel condominium and is not part of this application. The Development Rights on this property will be released simultaneously with the recording of the Final plat for this subdivision and such area will remain Common Elements of the Hotel Condominium unencumbered by Development Rights.

Separate development applications are expected to be submitted for multifamily condominium development on Lot 1 and aerial tramway and related facilities on the Tram Lot.





The subject property is approximately 4.31 acres in size. It is in the Northeast ¼ of Section 28, Township 6 North, Range 84 West of the 6th Principal Meridian, City of Steamboat Springs, Routt County, Colorado.

Specifically, the site is located in the center of Mount Werner Circle, south of the Steamboat Grand and north of the West Condominiums. The proposed construction will be limited to a disturbance area of approximately 5.94-acres below 7000-feet in elevation.

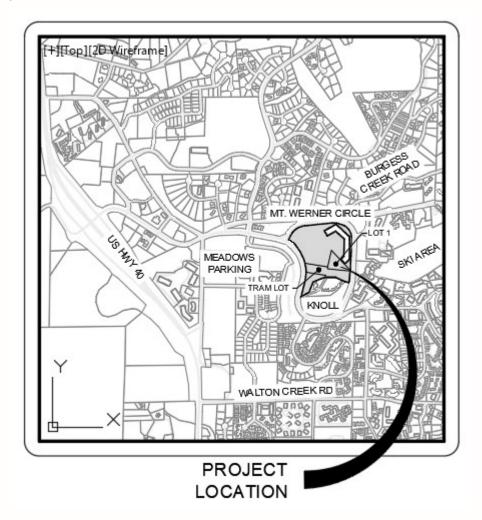


Figure 1- Vicinity Map

The existing site sits atop a knoll of native vegetation grasses. Cutting through the site are three (3) asphalt trails/accesses running generally north to south. The two on the east are pedestrian trails and the western asphalt access is an emergency access road for the Steamboat Grand. There also exists a gondola tram line with five (5) tram towers that runs east to west.

The project proposes the construction of a paved internal private access roadway to access lot 1, a paved emergency access to the Steamboat Grand, and over lot grading of Lot 1. One proposed water quality/detention facility will receive the runoff from the impervious and snowstorage surfaces.





DRAINAGE CRITERIA AND METHODOLOGY

Landmark prepared this report in accordance with *City of Steamboat Springs Engineering Standards, Section 5.0, Drainage Criteria* effective September 2007 and updated July 2019. The methods used by Landmark are described below and the actual calculations are presented in the Appendices. The scope of this report is limited to flow determinations related to the described hydrological storm event. This report does not attempt to model subsurface flows nor is it intended to be used in the design of structure features including foundation drains and roof drains.

Design Rainfall and Runoff Frequency

Landmark used the 5-year, 24-hour storm to analyze the minor storm event and the 100-year, 24-hour storm for the major storm event. Landmark used the Rational Method to determine peak runoff of small basins to design the on-site storm water runoff infrastructure associated with this project. The minimum time of concentration (t_c) used for this analysis is 5 minutes, based on the recommendations for urbanized watersheds found in Section 5.2.6.1 of the *Drainage Criteria*.

Storm Sewer Design

Storm sewers were designed and evaluated using Autodesk's Storm and Sanitary Sewer Analysis, which uses hydrodynamic routing. Storm sewers were sized to convey the minor storm event so that the HGL does not exceed the ground elevation however, the storm sewers convey the major storm event as well. In general, channels and roadside ditches are designed so that the Froude number during the major storm does not exceed 0.8.

Stormwater Quality

The project uses the WQCV design standard to provide stormwater quality treatment in the form of a sand filter designed per the parameters recommended in Volume 3 of the Mile High Flood District's Criteria Manual. This standard was chosen due to the expected low pollutant load and its widespread applicability.

EXISTING SITE CONDITIONS

The historic condition of the site is an undeveloped lot (4.35 acres) that is vacant and covered with native grasses. In this report the term "historic condition" refers to the conditions of the site prior to any construction activity and may also be referred to as the "pre-development condition" or "existing condition".

Figure 2: Existing Conditions shows the features of the site prior to development.

Currently the site is vacant (except for the three (3) asphalt surfaced trails/accesses) and covered by well-established native grasses, shrubs, and trees. The site slopes to the east and to the west from a large knoll which delineates the drainage.





The existing site is evaluated as two drainage basins. Basin H1 contains the west draining slopes of Lot 1 and the Tram Lot, as well as the westerly portion of the West Condominiums development. Basin H1 drainage is collected in a roadside ditch on the east side of Mt Werner Circle and routed into an existing 24" CMP culvert under Mt Werner Circle and outfalls into the Wildhorse Meadows subdivision, which ultimately outfalls to a storm sewer system under Ski Town Park and into the Yampa River.

Basin H2 contains the east draining slopes of Lot 1, and a portion of the grand building, Mt Werner Circle, and the West Condominiums. Basin H2 drainage is collected in a series of roadside ditches and culverts, which ultimately outfalls into Burgess Creek and from there into the Yampa River. Table 1 below summarizes the existing basin hydrology.

Table 1: Existing Basin Hydrology Summary							
					_		
Basin	Total Area (acres)	%lmp	C ₅	C ₁₀₀	T _c (min)	Q₅ (cfs)	Q ₁₀₀ (cfs)
H1	7.93	26%	0.28	0.56	15.03	5.08	22.05
H2	4.15	40%	0.35	0.58	16.54	3.09	11.23

A review of the NRCS soil data for the area indicates the site is dominated by NRCS HSG C soils which are soils having a slow infiltration rate when thoroughly wetted and consisting chiefly of soils with a layer that impedes downward movement of water or soils with moderately fine to fine texture. These soils have a slow rate of water transmission.

FEMA FLOODPLAIN

Landmark reviewed FEMA FIRM Community Panel Numbers 08107-CO883-D (February 4, 2005) and no portions of the property are within the 100yr and 500yr floodplains.

PROPOSED SITE CONDITIONS

This project proposes the construction of a paved internal private access roadway to access lot 1, a paved emergency access to the Steamboat Grand, and over lot grading of Lot 1. Lot 1 is expected to be developed for multifamily condominium and the Tram Lot is expected to be developed for an aerial tramway and related facilities. Table 6-3 from Urban Drainage for recommended percentage imperviousness values was used to estimate future development imperviousness. Lot 1 was assumed at 70% impervious (slightly less than the 75% recommended for "Apartments" as there will be small portions of the lot not developed due to steep slopes). The Tram Lot was assumed at 20% impervious (Conservative estimate for impervious improvements to include tram towers, access paths, and covered tram turn station). The total disturbed area (including all of Lot 1 and the Tram Lot) is expected to be about 5.94-acres. The proposed development is shown in Figure 3: Proposed Conditions.

The site is divided into 3 subbasins, D1.a, D1.b & D2. Basins D1.a & D1.b drain to the west and outfall to the culvert under Mt Werner Circle to the Wildhorse Meadows Subdivision. Basin D1.a consists of mainly existing, undisturbed areas, and a small portion of the proposed internal private access roadway. The proposed portion of basin D1.a will be routed into a proposed curb and gutter and roadside ditch, which





will outfall directly into the existing culvert under Mt Werner Circle. Basin D1.b consists of the remainder of the west draining developed areas which include the internal private access, emergency access, Lot 1 and the Tram Lot. Basin D1.b will be routed through swales and culverts to the proposed water quality/detention facility on the western side of the Tram Lot. The proposed facility will outfall into the existing culvert under Mt Werner Circle.

Basin D2 consists of east draining portions of Lot 1 and the Tram Lot. Drainage from these areas will remain historical as there is no proposed increase run-off.

Table 2 summarizes and compares the hydrological characteristics of the developed site and the existing site:

Table 2: Existing vs. Developed Basin Hydrology Summary								
Dania		1			1		T	
Basin	Total Area (acres)	%lmp	C ₅	C ₁₀₀	T _c (min)	Q₅ (cfs)	Q ₁₀₀ (cfs)	
H1	7.93	26%	0.28	0.56	15.03	5.08	22.05	
H2	4.15	40%	0.35	0.58	16.54	3.09	11.23	
D1.a	4.52	41%	0.35	0.58	17.24	3.35	12.05	
D1.b	4.98	39%	0.35	0.58	14.63	4.02	14.58	
D2	3.88	44%	0.37	0.59	16.54	3.06	10.70	

Design points DP-1.b.1 and DP-1.b.2 quantify the runoff to each curb inlet. Table 3 summarizes the design points for the developed site:

Table 3: Design Point Hydrology Summary							
		•					
Basin	Total Area (acres)	%lmp	C ₅	C ₁₀₀	T _c (min)	Q ₅ (cfs)	Q ₁₀₀ (cfs)
DP-1.b.1	0.16	62%	0.47	0.64	9.37	0.23	0.69
DP-1.b.2	0.11	100%	0.90	0.96	7.45	0.34	0.78





Detention

The proposed development will increase the imperviousness of the site to 39% in basin D1.b and 44% in basin D2, resulting in an increase in estimated peak runoff for both the minor and major storm in basin D1.b and a decrease in estimated peak runoff for both the minor and major storm in basin D2 as the size of the basin has been decreased (see Table 2). The pond in basin D1.b (pond WQ-1) will provide detention to restrict flows to historic values at H1. Table 4 summarized the detention release rates:

Table 4: Allowable Outflow for Detention Calculation						
Design						
Storm	Qн	Q _{UD}	\mathbf{Q}_{A}			
5-Year	5.08	3.35	1.73			
100-Year	22.05	12.05	10.00			

Q_H Historic peak flow (cfs)

Q_{UD} Undetained flow (cfs)

Q_A Allowable peak flow from detention facility (cfs)

The required volume estimates for the design storms are V₅=2,005-ft³ and V₁₀₀=4,028-ft³.

Table 5 in the next section summarizes the pond volumes and other parameters.

Storm System

Storm sewer systems in general will be made up of ADS drain basins and corrugated HDPE pipe in sizes from 12" to 24". The underdrains in the ponds will be 4" HDPE perforated pipe and the outlet structure's will be CDOT type C inlets. All basin, storm-system, swale, and water quality calculations are included in the appendices.

STORMWATER QUALITY

Water quality in the Yampa River is degraded by the washing-off of accumulated deposits on the urban landscape of Steamboat Springs. Metals, salts, sand, gravel, trash, debris, and organics (including oil and gasoline) all accumulate on the streets and in parking lots of Steamboat Springs over the course of time. During a rainstorm event, these pollutants are washed into the Yampa River and its tributaries. Water quality problems caused by these pollutants include turbid water, nutrient enrichment, bacterial contamination, reduction in dissolved oxygen, and increased stress on aquatic life. The most prevalent pollutant in Steamboat Springs is sediment. BMP's included in this project are designed to minimize the amount of sediment leaving the site and entering the waterways.

Potential Pollutant Sources: The following are anticipated pollutant sources for this project:

- 1. Routine maintenance involving fertilizers, pesticides, detergents, fuels, solvents, oils, etc.
- 2. On site waste management practices (waste piles, dumpsters, etc.)

BMP Selection:

From the Mile High Flood District's (MHFD) *Urban Storm Drainage Criteria Manual* (USDCM), Volume 3, BMP selection involves many factors such as physical site characteristics, treatment objectives, aesthetics, safety, maintenance requirements, and costs. As each site is unique, there is not a standard BMP that can





be implemented for every application and therefore there may be multiple solutions including standalone BMPs or 'treatment trains' that combine multiple BMPs to achieve the water quality objectives.

Water Quality Capture Volume:

The water quality capture volume (WQCV) is calculated following Section 5.12.7.1 of the *Design Criteria*. A drain time coefficient of 0.8 is used, based on the MHFD's recommended minimum drain time of 12 hours for SF's.

Table 5 summarizes the requirements and designs of the Water Quality Ponds:

Table 5: Water Quality / Detention Pond Summary								
Basin	Sand Filter Flat Area (ft²)		WQCV ¹ (ft³)	Detention ² V ₅ (ft ³)	Detention ² V ₁₀₀ (ft ³)	V ₁₀₀ + WQCV (ft³)	Total Volume (ft³)	
	Required	Provided		Req	uired		Provided	
WQ-1	1059	1,113	2,433	2,005	4,028	6,461	6,481	
				Total Treated Area (acres) 4.98				
			Total Disturbed area (acres) 5.94					
				Percent 1	reated (%)		84%	

These facilities treat approximately 84% of the site leaving 0.96-acres, or 16% of the site area untreated. A separate water quality facility for a portion of basin D2 is not feasible as it would require locating the treatment pond on a steep slope or within the right-of-way near the Gondola Transit Center that is currently looking to redevelop.

The calculations for the WQCV and BMP sizing have been included in the appendices.

Site operation can significantly manage stormwater quality and care should be exercised to monitor and maintain the BMPs described. An Operation and Maintenance Plan is included in Appendix D (with final drainage study).

CONCLUSIONS

The improvements for the proposed development include the construction of a paved internal private access roadway to access lot 1, a paved emergency access to the Steamboat Grand, and over lot grading of Lot 1, and one water quality (sand filter)/ detention pond.

Runoff from the project will maintain historical drainage patterns with all flow discharging to the existing culvert under Mt Werner Circle to the west and to the existing roadside ditch to the east.

The runoff from developed areas will be treated in the sand filter. Although the proposed development will increase the estimated peak flows from the site, the sand filter pond will also provide detention for the project by restricting flows to historic values.

In order to operate as intended, on-going maintenance and inspection of storm systems, swales and the sand filters will be required.





LIMITATIONS

This study is intended to estimate and analyze peak stormwater runoff volumes generated by hydrologic events in order to evaluate existing drainage infrastructure and design new infrastructure needed to manage these flows. It does not account for groundwater, springs, or seeps and is not intended to be used for the evaluation or design of foundation drains or roof drains.

Basin delineations, areas, and soil characteristics are based on those described in the Report. Actual conditions may vary. Landmark's assumptions, recommendations and opinions are based on this information and the proposed site plan. If any of the data is found to be inaccurate or the proposed site plan is changed, Landmark should be contacted to review this report and make any necessary revisions.

The data, opinions, and recommendations of this report are applicable to the specific design elements and location that is the subject of this report. This report is not applicable to any other design elements or to any other locations. Any and subsequent users accept any and all liability resulting from any use or reuse of the data, opinions, and recommendation without the prior written consent of Landmark Consultants, Inc.

Landmark Consultants, Inc. has no responsibility for construction means, methods, techniques, sequences, or procedures, or for safety precautions or programs in connection with the construction, for the acts or omissions of the contractor, or any other person performing any of the construction, or for the failure of any of them to carry out the construction in accordance with the Final Construction Drawings and Specifications.

The only warranty or guarantee made by Landmark Consultants, Inc. in connection with the services performed for this project is that such services are performed with the care and skill ordinarily exercised by members of the profession practicing under similar conditions, at the same time, and in the same or similar locality. No other warranty, expressed or implied, is made or intended by rendering such services or by furnishing written reports of the findings.





REFERENCES

- 1. <u>Section 5.0 Drainage Criteria</u>, City of Steamboat Springs Department of Public Works, July 2019.
- 2. <u>Drainage Criteria Manual (Volumes 1 3)</u>, Mile High Flood District's (MHFD), 2019
- 3. <u>Hydraulic Design of Energy Dissipators for Culverts and Channels (HEC 14)</u>, Federal Highway Administration, September 1983
- 4. <u>Hydraulic Design of Highway Culverts (HDS-5)</u>, Federal Highway Administration, September 2001
- 5. Procedures for Determining Peak Flows in Colorado, Natural Resource Conservation Service, 1984
- 6. <u>Urban Hydrology for Small Watersheds (TR-55)</u>, Natural Resource Conservation Service, June 1986
- 7. <u>Citywide Stormwater Master Plan</u>, City of Steamboat Springs, Colorado, SEH, March 2013.





APPENDIX A

HYDROLOGIC CALCULATIONS

Runoff Chapter 6

Table 6-3. Recommended percentage imperviousness values

Land Use or	Percentage Imperviousness
Surface Characteristics	(%)
Business:	
Downtown Areas	95
Suburban Areas	75
Residential lots (lot area only):	-
Single-family	
2.5 acres or larger	12
0.75 – 2.5 acres	20
0.25 - 0.75 acres	30
0.25 acres or less	45
Apartments	75
Industrial:	
Light areas	80
Heavy areas	90
Parks, cemeteries	10
Playgrounds	25
Schools	55
Railroad yard areas	50
Undeveloped Areas:	·
Historic flow analysis	2
Greenbelts, agricultural	2
Off-site flow analysis (when land use not defined)	45
Streets:	
Paved	100
Gravel (packed)	40
Drive and walks	90
Roofs	90
Lawns, sandy soil	2
Lawns, clayey soil	2

Runoff Chapter 6

Table 6-5. Runoff coefficients, c

Total or Effective			NRCS Hydr	ologic Soil	Group A		
% Impervious	2-Year	5-Year	10-Year	25-Year	50-Year	100-Vear	500-Year
2%	0.01	0.01	0.01	0.01	0.04	0.13	0.27
5%	0.02	0.02	0.02	0.03	0.07	0.15	0.29
10%	0.02	0.02	0.05	0.07	0.11	0.19	0.32
15%	0.07	0.08	0.08	0.07	0.11	0.13	0.35
20%	0.07	0.11	0.12	0.14	0.13	0.23	0.38
25%	0.14	0.11	0.12	0.19	0.24	0.27	0.42
30%	0.14	0.19	0.10	0.13	0.24	0.34	0.42
35%	0.18	0.13	0.24	0.23	0.28	0.34	0.48
40%	0.21	0.23	0.24	0.27	0.32	0.38	0.48
45%	0.23	0.27	0.28	0.36	0.37	0.42	0.54
50%	0.34	0.31	0.33	0.36	0.41	0.46	0.54
				0.41			
55%	0.39	0.4	0.42		0.49	0.54	0.61
60%	0.43	0.45	0.47	0.5	0.54	0.58	0.64
65%	0.48	0.5	0.51	0.54	0.58	0.62	0.67
70%	0.53	0.55	0.56	0.59	0.62	0.65	0.71
75%	0.58	0.6	0.61	0.64	0.66	0.69	0.74
80%	0.63	0.65	0.66	0.69	0.71	0.73	0.77
85%	0.68	0.7	0.71	0.74	0.75	0.77	0.8
90%	0.73	0.75	0.77	0.79	0.79	0.81	0.84
95%	0.79	0.81	0.82	0.83	0.84	0.85	0.87
100%	0.84	0.86	0.87	0.88	0.88	0.89	0.9
Total or Effective		1	NRCS Hydr			T	
% Impervious	2-Year	5-Year	10-Year	25-Year	50-Year	100 17	=00 T7
						100-Year	500-Year
2%	0.01	0.01	0.07	0.26	0.34	0.44	0.54
2% 5%	0.01 0.03	0.01 0.03	0.07 0.1	0.26 0.28	0.34 0.36	0.44 0.45	0.54 0.55
2% 5% 10%	0.01 0.03 0.06	0.01 0.03 0.07	0.07 0.1 0.14	0.26 0.28 0.31	0.34 0.36 0.38	0.44 0.45 0.47	0.54 0.55 0.57
2% 5%	0.01 0.03 0.06 0.09	0.01 0.03 0.07 0.11	0.07 0.1 0.14 0.18	0.26 0.28 0.31 0.34	0.34 0.36 0.38 0.41	0.44 0.45 0.47 0.5	0.54 0.55 0.57 0.59
2% 5% 10% 15% 20%	0.01 0.03 0.06	0.01 0.03 0.07	0.07 0.1 0.14 0.18 0.22	0.26 0.28 0.31 0.34 0.38	0.34 0.36 0.38 0.41 0.44	0.44 0.45 0.47	0.54 0.55 0.57
2% 5% 10% 15% 20% 25%	0.01 0.03 0.06 0.09 0.13 0.17	0.01 0.03 0.07 0.11 0.15 0.19	0.07 0.1 0.14 0.18 0.22 0.26	0.26 0.28 0.31 0.34 0.38 0.41	0.34 0.36 0.38 0.41	0.44 0.45 0.47 0.5	0.54 0.55 0.57 0.59
2% 5% 10% 15% 20%	0.01 0.03 0.06 0.09 0.13	0.01 0.03 0.07 0.11 0.15	0.07 0.1 0.14 0.18 0.22 0.26 0.3	0.26 0.28 0.31 0.34 0.38	0.34 0.36 0.38 0.41 0.44	0.44 0.45 0.47 0.5 0.52	0.54 0.55 0.57 0.59 0.61
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2% 5% 10% 15% 20% 25% 30%	0.01 0.03 0.06 0.09 0.13 0.17 0.2	0.01 0.03 0.07 0.11 0.15 0.19 0.23	0.07 0.1 0.14 0.18 0.22 0.26 0.3	0.26 0.28 0.31 0.34 0.38 0.41 0.44	0.34 0.36 0.38 0.41 0.44 0.47 0.49	0.44 0.45 0.47 0.5 0.52 0.54 0.57	0.54 0.55 0.57 0.59 0.61 0.63 0.65
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2% 5% 10% 15% 20% 25% 30% 35% 40%	0.01 0.03 0.06 0.09 0.13 0.17 0.2 0.24 0.29	0.01 0.03 0.07 0.11 0.15 0.19 0.23 0.27 0.32	0.07 0.1 0.14 0.18 0.22 0.26 0.3 0.34 0.38	0.26 0.28 0.31 0.34 0.38 0.41 0.44 0.47 0.5	0.34 0.36 0.38 0.41 0.44 0.47 0.49 0.52 0.55	0.44 0.45 0.47 0.5 0.52 0.54 0.57 0.59 0.61	0.54 0.55 0.57 0.59 0.61 0.63 0.65 0.66 0.68
2% 5% 10% 15% 20% 25% 30% 35% 40% 45%	0.01 0.03 0.06 0.09 0.13 0.17 0.2 0.24 0.29 0.33	0.01 0.03 0.07 0.11 0.15 0.19 0.23 0.27 0.32 0.36	0.07 0.1 0.14 0.18 0.22 0.26 0.3 0.34 0.38 0.42	0.26 0.28 0.31 0.34 0.38 0.41 0.44 0.47 0.5 0.53	0.34 0.36 0.38 0.41 0.44 0.47 0.49 0.52 0.55 0.58	0.44 0.45 0.47 0.5 0.52 0.54 0.57 0.59 0.61 0.64	0.54 0.55 0.57 0.59 0.61 0.63 0.65 0.66 0.68 0.7
2% 5% 10% 15% 20% 25% 30% 35% 40% 45% 50%	0.01 0.03 0.06 0.09 0.13 0.17 0.2 0.24 0.29 0.33 0.37	0.01 0.03 0.07 0.11 0.15 0.19 0.23 0.27 0.32 0.36 0.4	0.07 0.1 0.14 0.18 0.22 0.26 0.3 0.34 0.38 0.42 0.46	0.26 0.28 0.31 0.34 0.38 0.41 0.44 0.47 0.5 0.53 0.56	0.34 0.36 0.38 0.41 0.44 0.47 0.49 0.52 0.55 0.58 0.61	0.44 0.45 0.47 0.5 0.52 0.54 0.57 0.59 0.61 0.64 0.66	0.54 0.55 0.57 0.59 0.61 0.63 0.65 0.66 0.68 0.7 0.72
2% 5% 10% 15% 20% 25% 30% 35% 40% 45% 50% 55%	0.01 0.03 0.06 0.09 0.13 0.17 0.2 0.24 0.29 0.33 0.37 0.42	0.01 0.03 0.07 0.11 0.15 0.19 0.23 0.27 0.32 0.36 0.4 0.45	0.07 0.1 0.14 0.18 0.22 0.26 0.3 0.34 0.38 0.42 0.46 0.5	0.26 0.28 0.31 0.34 0.38 0.41 0.44 0.47 0.5 0.53 0.56 0.6	0.34 0.36 0.38 0.41 0.44 0.47 0.49 0.52 0.55 0.58 0.61 0.63	0.44 0.45 0.47 0.5 0.52 0.54 0.57 0.59 0.61 0.64 0.66 0.68	0.54 0.55 0.57 0.59 0.61 0.63 0.65 0.66 0.68 0.7 0.72 0.74
2% 5% 10% 15% 20% 25% 30% 35% 40% 45% 50% 55% 60%	0.01 0.03 0.06 0.09 0.13 0.17 0.2 0.24 0.29 0.33 0.37 0.42 0.46	0.01 0.03 0.07 0.11 0.15 0.19 0.23 0.27 0.32 0.36 0.4 0.45 0.49	0.07 0.1 0.14 0.18 0.22 0.26 0.3 0.34 0.38 0.42 0.46 0.5 0.54	0.26 0.28 0.31 0.34 0.38 0.41 0.44 0.47 0.5 0.53 0.56 0.6 0.63	0.34 0.36 0.38 0.41 0.44 0.47 0.49 0.52 0.55 0.58 0.61 0.63 0.66	0.44 0.45 0.47 0.5 0.52 0.54 0.57 0.59 0.61 0.64 0.66 0.68 0.71	0.54 0.55 0.57 0.59 0.61 0.63 0.65 0.66 0.68 0.7 0.72 0.74 0.76
2% 5% 10% 15% 20% 25% 30% 35% 40% 45% 50% 55% 60% 65%	0.01 0.03 0.06 0.09 0.13 0.17 0.2 0.24 0.29 0.33 0.37 0.42 0.46 0.5	0.01 0.03 0.07 0.11 0.15 0.19 0.23 0.27 0.32 0.36 0.4 0.45 0.49 0.54	0.07 0.1 0.14 0.18 0.22 0.26 0.3 0.34 0.38 0.42 0.46 0.5 0.54 0.58	0.26 0.28 0.31 0.34 0.38 0.41 0.44 0.47 0.5 0.53 0.66 0.63 0.66	0.34 0.36 0.38 0.41 0.44 0.47 0.49 0.52 0.55 0.58 0.61 0.63 0.66 0.69	0.44 0.45 0.47 0.5 0.52 0.54 0.57 0.69 0.61 0.64 0.66 0.68 0.71 0.73	0.54 0.55 0.57 0.59 0.61 0.63 0.65 0.66 0.7 0.72 0.74 0.76 0.77
2% 5% 10% 15% 20% 25% 30% 35% 40% 45% 50% 55% 60% 65% 70%	0.01 0.03 0.06 0.09 0.13 0.17 0.2 0.24 0.29 0.33 0.37 0.42 0.46 0.5 0.55	0.01 0.03 0.07 0.11 0.15 0.19 0.23 0.27 0.32 0.36 0.4 0.45 0.49 0.54	0.07 0.1 0.14 0.18 0.22 0.26 0.3 0.34 0.38 0.42 0.46 0.5 0.54 0.58 0.62	0.26 0.28 0.31 0.34 0.38 0.41 0.44 0.47 0.5 0.53 0.66 0.63 0.66 0.69	0.34 0.36 0.38 0.41 0.44 0.47 0.49 0.52 0.55 0.61 0.63 0.66 0.69 0.72	0.44 0.45 0.47 0.5 0.52 0.54 0.57 0.59 0.61 0.64 0.66 0.68 0.71 0.73 0.75	0.54 0.55 0.57 0.59 0.61 0.63 0.65 0.66 0.7 0.72 0.74 0.76 0.77 0.79
2% 5% 10% 15% 20% 25% 30% 35% 40% 45% 50% 55% 60% 65% 70% 75%	0.01 0.03 0.06 0.09 0.13 0.17 0.2 0.24 0.29 0.33 0.37 0.42 0.46 0.5 0.6	0.01 0.03 0.07 0.11 0.15 0.19 0.23 0.27 0.32 0.36 0.4 0.45 0.49 0.54 0.58 0.63	0.07 0.1 0.14 0.18 0.22 0.26 0.3 0.34 0.38 0.42 0.46 0.5 0.54 0.58 0.62 0.66	0.26 0.28 0.31 0.34 0.38 0.41 0.47 0.5 0.53 0.66 0.63 0.66 0.69 0.72	0.34 0.36 0.38 0.41 0.44 0.47 0.49 0.52 0.55 0.68 0.61 0.63 0.66 0.69 0.72 0.75	0.44 0.45 0.47 0.5 0.52 0.54 0.57 0.59 0.61 0.64 0.66 0.68 0.71 0.73 0.75 0.78	0.54 0.55 0.57 0.59 0.61 0.63 0.65 0.66 0.7 0.72 0.74 0.76 0.77 0.79 0.81
2% 5% 10% 15% 20% 25% 30% 35% 40% 45% 50% 55% 60% 65% 70% 75% 80%	0.01 0.03 0.06 0.09 0.13 0.17 0.2 0.24 0.29 0.33 0.37 0.42 0.46 0.5 0.55 0.6 0.64	0.01 0.03 0.07 0.11 0.15 0.19 0.23 0.27 0.32 0.36 0.4 0.45 0.49 0.54 0.58 0.63 0.67	0.07 0.1 0.14 0.18 0.22 0.26 0.3 0.34 0.38 0.42 0.46 0.5 0.54 0.58 0.62 0.66 0.7	0.26 0.28 0.31 0.34 0.38 0.41 0.44 0.47 0.5 0.53 0.66 0.63 0.66 0.69 0.72 0.75	0.34 0.36 0.38 0.41 0.44 0.47 0.49 0.52 0.55 0.68 0.61 0.63 0.66 0.69 0.72 0.75 0.77	0.44 0.45 0.47 0.5 0.52 0.54 0.57 0.59 0.61 0.64 0.66 0.71 0.73 0.75 0.78 0.82	0.54 0.55 0.57 0.59 0.61 0.63 0.65 0.66 0.7 0.72 0.74 0.76 0.77 0.79 0.81 0.83
2% 5% 10% 15% 20% 25% 30% 35% 40% 45% 50% 55% 60% 65% 70% 75% 80% 85%	0.01 0.03 0.06 0.09 0.13 0.17 0.2 0.24 0.29 0.33 0.37 0.42 0.46 0.5 0.64 0.69	0.01 0.03 0.07 0.11 0.15 0.19 0.23 0.27 0.32 0.36 0.4 0.45 0.49 0.54 0.58 0.63 0.67 0.72	0.07 0.1 0.14 0.18 0.22 0.26 0.3 0.34 0.38 0.42 0.46 0.5 0.54 0.58 0.62 0.66 0.7 0.74	0.26 0.28 0.31 0.34 0.38 0.41 0.44 0.47 0.5 0.53 0.66 0.63 0.66 0.69 0.72 0.78	0.34 0.36 0.38 0.41 0.44 0.47 0.49 0.52 0.55 0.58 0.61 0.63 0.66 0.69 0.72 0.75 0.77 0.8	0.44 0.45 0.47 0.5 0.52 0.54 0.57 0.59 0.61 0.64 0.66 0.71 0.73 0.75 0.78 0.8	0.54 0.55 0.57 0.59 0.61 0.63 0.65 0.66 0.7 0.72 0.74 0.76 0.77 0.79 0.81 0.83 0.85

Chapter 6 Runoff

Table 6-5.	Runoff	coefficients,	c ((continued)

Total or Effective	NRCS Hydrologic Soil Group C						
% Impervious	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year	500-Year
2%	0.01	0.05	0.15	0.33	0.40	0.49	0.59
5%	0.03	0.08	0.17	0.35	0.42	0.5	0.6
10%	0.06	0.12	0.21	0.37	0.44	0.52	0.62
15%	0.1	0.16	0.24	0.4	0.47	0.55	0.64
20%	0.14	0.2	0.28	0.43	0.49	0.57	0.65
25%	0.18	0.24	0.32	0.46	0.52	0.59	0.67
30%	0.22	0.28	0.35	0.49	0.54	0.61	0.68
35%	0.26	0.32	0.39	0.51	0.57	0.63	0.7
40%	0.3	0.36	0.43	0.54	0.59	0.65	0.71
45%	0.34	0.4	0.46	0.57	0.62	0.67	0.73
50%	0.38	0.44	0.5	0.6	0.64	0.69	0.75
55%	0.43	0.48	0.54	0.63	0.66	0.71	0.76
60%	0.47	0.52	0.57	0.65	0.69	0.73	0.78
65%	0.51	0.56	0.61	0.68	0.71	0.75	0.79
70%	0.56	0.61	0.65	0.71	0.74	0.77	0.81
75%	0.6	0.65	0.68	0.74	0.76	0.79	0.82
80%	0.65	0.69	0.72	0.77	0.79	0.81	0.84
85%	0.7	0.73	0.76	0.79	0.81	0.83	0.86
90%	0.74	0.77	0.79	0.82	0.84	0.85	0.87
95%	0.79	0.81	0.83	0.85	0.86	0.87	0.89
100%	0.83	0.85	0.87	0.88	0.89	0.89	0.9

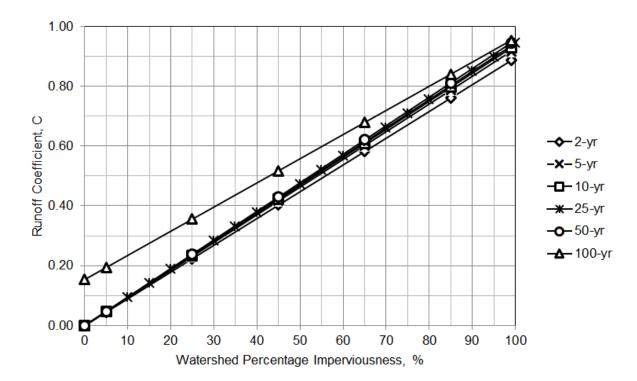


Figure 6-1. Runoff coefficient vs. watershed imperviousness NRCS HSG A

Runoff Chapter 6

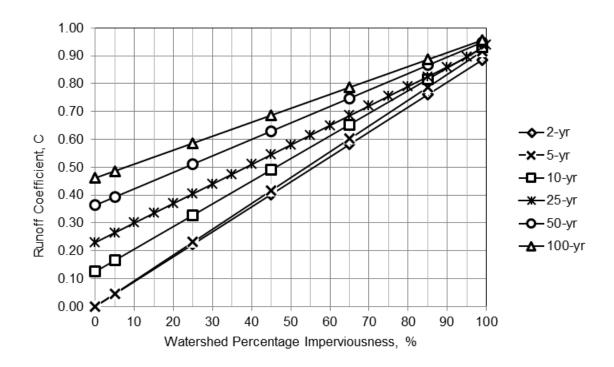


Figure 6-2. Runoff coefficient vs. watershed imperviousness NRCS HSG B

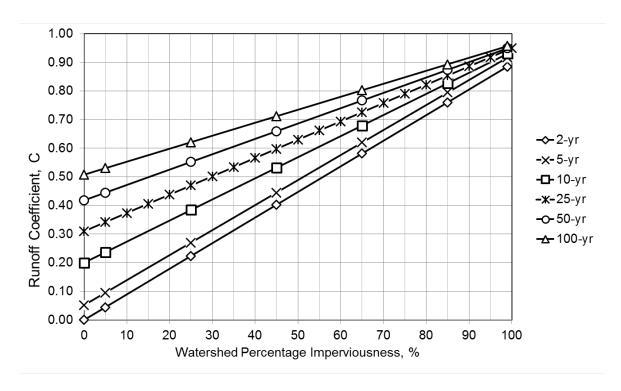
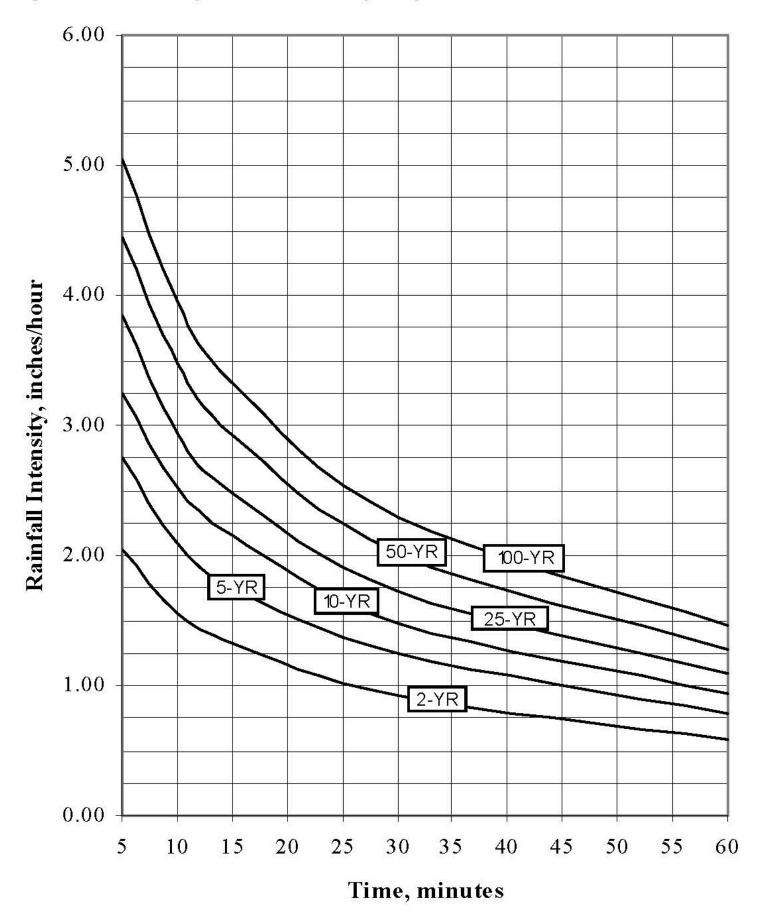
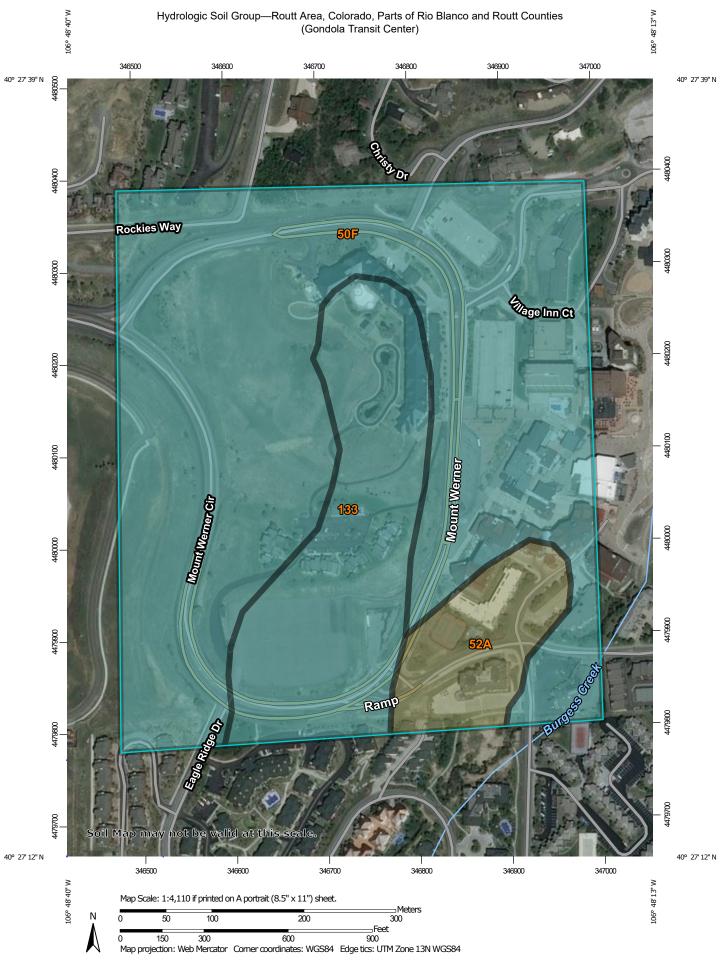


Figure 6-3. Runoff coefficient vs. watershed imperviousness NRCS HSG C and D

Figure 5.5.1 Intensity – Duration – Frequency Curves





MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D **Soil Rating Polygons** Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D Streams and Canals contrasting soils that could have been shown at a more detailed Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. Soil Survey Area: Routt Area, Colorado, Parts of Rio Blanco and Routt Counties Survey Area Data: Version 11, Sep 2, 2021 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: May 8, 2012—Oct 5. **Soil Rating Points** The orthophoto or other base map on which the soil lines were A/D compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

Hydrologic Soil Group

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
50F	Routt loam, 25 to 65 percent slopes, very stony	С	53.8	70.3%
52A	Slocum loam, 0 to 3 percent slopes	C/D	6.3	8.2%
133	Lintim loam, 3 to 25 percent slopes	С	16.4	21.4%
Totals for Area of Interes	est	1	76.5	100.0%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified

Tie-break Rule: Higher



Lawns and Landscaping

Assumed Imperviousness (Lot 1)

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ESIGNER:	Matthew Eggen	
DATE:	10/5/2022	
POND ID:		

BASIN RUNOFF COEFFICIENT CAL										
	Percent									
Character of Surface	Impervious	IDF	Soil Type							
Asphalt Parking and Walkways	100%	Steamboat Springs NOA	AA C							
Gravel	40%	<u>-</u>		-						
Roof	90%									

2% 70%

Assumed Im	nperviousness (Tr	am Lot)	20%	-													
			Area of Asphalt	Area of Asphalt	Area of	Area of			Area of	Area of						5-year	100-year
			Parking and	Parking and	Gravel	Gravel	Area of	Area of	Lawns and	Lawns and	Assumed	Assumed	Assumed	Assumed		Composite	Composite
	Basin Area	Basin Area	Walkways	Walkways	Surfaces	Surfaces	Roof	Roof	Landscaping	Landscaping	Imperviousness	Imperviousness	Imperviousness	Imperviousness	Percent	Runoff	Runoff
Basin ID	(sq.ft.)	(acres)	(sq.ft.)	(acres)	(sq.ft)	(acres)	(sq.ft.)	(acres)	(sq.ft.)	(acres)	(sq.ft.)	(acres)	(sq.ft.)	(acres)	Impervious	Coefficient	Coefficient
H1	345352.00	7.93	75723.00	1.74	0.00	0.00	9030.00	0.21	260599.00	5.98	0.00	0.00	0.00	0.00	26%	0.28	0.56
H2	180657.00	4.15	35221.00	0.81	0.00	0.00	37954.00	0.87	107482.00	2.47	0.00	0.00	0.00	0.00	40%	0.35	0.58
D1.a	196915.00	4.52	67041.80	1.54	0.00	0.00	9030.00	0.21	105065.20	2.41	0.00	0.00	15778.00	0.36	41%	0.35	0.58
D1.b	216849.00	4.98	19955.00	0.46	0.00	0.00	6682.00	0.15	51830.00	1.19	60090.00	1.38	78292.00	1.80	39%	0.35	0.58
DP-1.b.1	7153.00	0.16	4353.00	0.10	0.00	0.00	0.00	0.00	2800.00	0.06	0.00	0.00	0.00	0.00	62%	0.47	0.64
DP-1.b.2	4821.00	0.11	4821.00	0.11	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	100%	0.90	0.96
D2	169168.00	3.88	32821.00	0.75	0.00	0.00	37954.00	0.87	73159.00	1.68	2484.00	0.06	22750.00	0.52	44%	0.37	0.59



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DATE:	10/5/2022
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BASIN TIME OF CONCENTRATION CALCULATIONS

Overland Flow, Time of Concentration:

(Equation RO-3)

 $T = \frac{0.395(1.1 - C_5)\sqrt{L}}{\text{Gutter/Swale Flow, Time of Concentration:}}$ (Equation RO-3

 $T_{t} = L / 60V$

T_c = T_i + T_t (Equation RO-2) Intensity, i From Figures 3.3.1-2 (Area II)

Velocity (Gutter Flow), V = 20·S^{1/2}

Velocity (Swale Flow), V = 15·S^{1/2}

Rational Equation: Q = CiA (Equation RO-1)

Kational Equal	1011. Q - C	IA (⊏quation	I KO-1)																				
		Overland F	nd Flow 1 Overland Flow 2			Conveyance Swale Flow 1		Conveyance Swale Flow 2				Time of Concentration											
				_				_ [_						_	Comp.	I	Actual
		Length, L	Slope, S	T _i		Length, L	Slope, S	Ti			Length, L	Slope, S	Velocity, V	T _t			Length, L	Slope, S	Velocity, V	T _t	T _c	$\frac{L}{100} + 10$	T _c
Basin(s)	C ₅ *	(ft)	(%)	(min)	C ₅	(ft)	(%)	(min)		K	(ft)	(%)	(ft/s)	(min)		K	(ft)	(%)	(ft/s)	(min)	(min)	180	(min)
H1	0.28	113	0.29	24.03	0.28		N/A	N/A	Short Pasture and Lawns	7	404	0.04	0.40	48.34	Short Pasture and Lawns	7	388	0.18	0.84	21.91	94.27	15.03	15.03
H2	0.35		N/A	N/A	0.35		N/A	N/A	Shallow Paved Swales	20	726	0.04	0.39	30.97	Short Pasture and Lawns	7	451	0.04	0.42	51.59	82.56	16.54	16.54
D1.a	0.35	0	0.00	N/A	0.35		N/A	N/A	Shallow Paved Swales	20	809	0.05	0.46	29.21	Short Pasture and Lawns	7	494	0.04	0.38	61.11	90.32	17.24	17.24
D1.b	0.35	100	0.13	27.29	0.35		N/A	N/A	Shallow Paved Swales	20	334	0.07	0.52	10.68	Shallow Paved Swales	20	400	0.02	0.26	25.57	63.53	14.63	14.63
DP-1.b.1	0.47	0	0.13	N/A	0.47		N/A	N/A	Short Pasture and Lawns	7	109	0.13	0.71	7.29	Shallow Paved Swales	20	70	0.08	0.56	2.08	9.37	10.99	9.37
DP-1.b.2	0.90	0	0.00	N/A	0.90		N/A	N/A	Shallow Paved Swales	20	241	0.07	0.54	7.45	Short Pasture and Lawns	7	0	0.00	N/A	N/A	7.45	11.34	7.45
D2	0.37		N/A	N/A	0.37		N/A	N/A	Shallow Paved Swales	20	726	0.04	0.39	30.97	Short Pasture and Lawns	7	451	0.04	0.42	51.59	82.56	16.54	16.54

Note: C_5 for overland flow is C value for that segment of flow, not overall basin C_5



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DIRECT RUNOFF COMPUTATIONS

Overland Flow, Time of Concentration:

Overland Flow, Time of Conce

$$T_i = \frac{0.395(1.1 - C_5)\sqrt{L}}{1/L}$$

(Equation RO-3)

Gutter/Swale Flow, Time of Concentration:

T_t = L / 60V

 $T_c = T_i + T_t$ (Equation RO-2)

Intensity, I from Fig. RA-2

(Equation RO-4)

Velocity (Gutter Flow), V = 20·S^{1/2} Velocity (Swale Flow), V = 15·S^{1/2}

Rational Equation: Q = CiA (Equation RO-1)

	and a first to the second of t											
Basin(s)	Area, A (acres)	T _c (min)	C ₅	C ₁₀₀	Intensity, I ₅	Intensity, I ₁₀₀	Flow, Q ₅ (cfs)	Q₅ per Acre (cfs/ac)	Flow, Q ₁₀₀ (cfs)	Q ₁₀₀ per Acre (cfs/ac)		
H1	7.93	15.03	0.28	0.56	2.27	4.96	5.08	0.64	22.05	2.78		
H2	4.15	16.54	0.35	0.58	2.14	4.68	3.09	0.75	11.23	2.71		
D1.a	4.52	17.24	0.35	0.58	2.10	4.59	3.35	0.74	12.05	2.67		
D1.b	4.98	14.63	0.35	0.58	2.32	5.06	4.02	0.81	14.58	2.93		
DP-1.b.1	0.16	9.37	0.47	0.64	3.01	6.56	0.23	1.41	0.69	4.17		
DP-1.b.2	0.11	7.45	0.90	0.96	3.38	7.37	0.34	3.04	0.78	7.07		
D2	3.88	16.54	0.37	0.59	2.14	4.68	3.06	0.79	10.70	2.75		



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PROJECT:	2571-001
DESIGNER:	Matthew Eggen
DATE:	10/5/2022
POND ID:	

TABLES

	Table 1: Basin Hydrology Summary											
Basin	Total Area (acres)	%lmp	C ₅	C ₁₀₀	T _c (min)	Q ₅ (cfs)	Q ₁₀₀ (cfs)					
H1	7.93	26%	0.28	0.56	15.03	5.08	22.05					
H2	4.15	40%	0.35	0.58	16.54	3.09	11.23					
D1.a	4.52	41%	0.35	0.58	17.24	3.35	12.05					
D1.b	4.98	39%	0.35	0.58	14.63	4.02	14.58					
DP-1.b.1	0.16	62%	0.47	0.64	9.37	0.23	0.69					
DP-1.b.2	0.11	100%	0.90	0.96	7.45	0.34	0.78					
D2	3.88	44%	0.37	0.59	16.54	3.06	10.70					

Allowable Outflow for Detention Calculation

Design Storm	Q _H	Q _{UD}	Q_A		
5-Year	5.08	3.35	1.73		
100-Year	22.05	12.05	10.00		

Q_H Historic peak flow (cfs)

 $Q_{\text{UD}}\,$ Undetained flow (cfs)

 Q_A Allowable peak flow from detention facility (cfs)

	Bioretention Pond Summary											
Basin	Sand Filter Flat Area (ft ²)		Flat Area $\begin{array}{ c c c c c c c c c c c c c c c c c c c$									
	Required	Provided		Re	Provided							
WQ-1	1059	1,113	2,433	2,005	4,028	6,461	6,481					
Total Treated Area (acres)						es)	4.98					
				Total Distur	5.94							
				Percent	Treated (%)	·	84%					



APPENDIX B

HYDRAULIC CALCULATIONS

Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Oct 3 2022

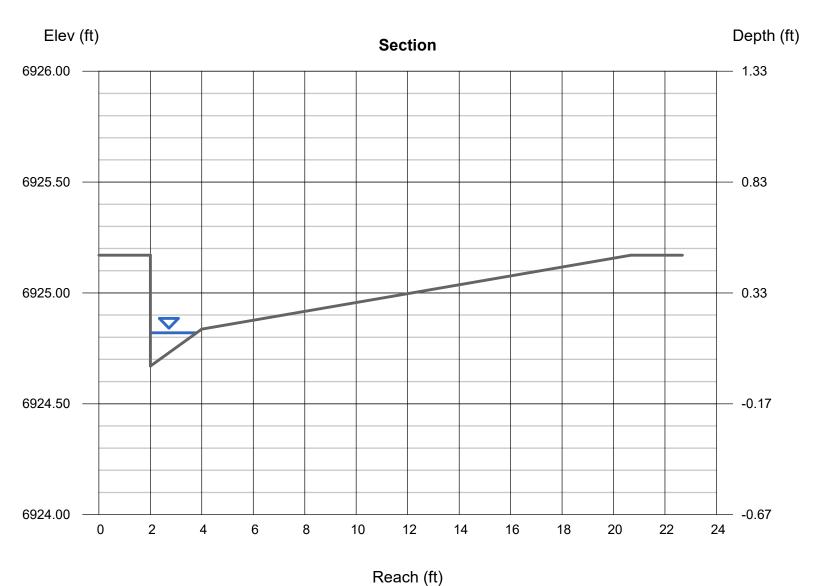
GutterAnalysis-DP-1.b.1

Gutter	
Cross SI, Sx (ft/ft)	= 0.020
Cross SI, Sw (ft/ft)	= 0.083
Gutter Width (ft)	= 2.00
Invert Elev (ft)	= 6924.67
Slope (%)	= 7.00
N-Value	= 0.015

Calculations

Compute by: Q vs Depth No. Increments = 50

Highlighted		
Depth (ft)	=	0.15
Q (cfs)	=	0.748
Area (sqft)	=	0.14
Velocity (ft/s)	=	5.54
Wetted Perim (ft)	=	1.96
Crit Depth, Yc (ft)	=	0.25
Spread Width (ft)	=	1.80
EGL (ft)	=	0.63



Channel Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Monday, Oct 3 2022

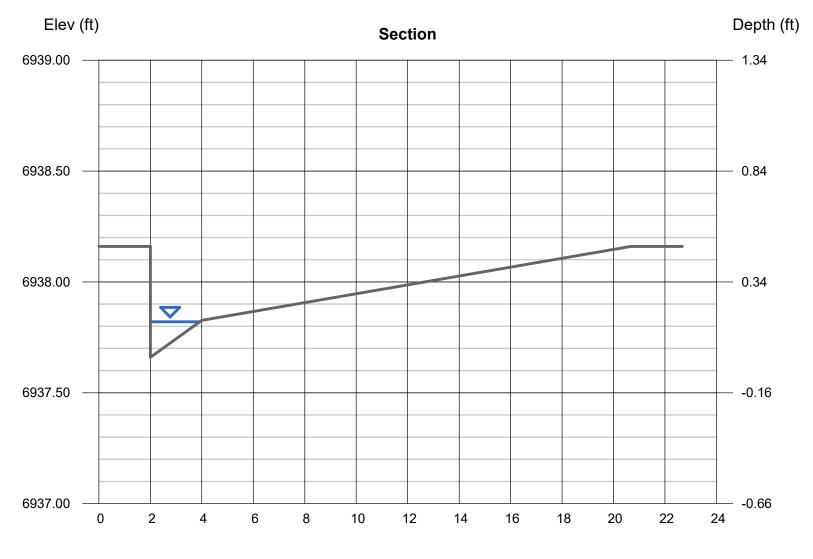
GutterAnalysis-DP-1.b.2

Gutter	
Cross SI, Sx (ft/ft)	= 0.020
Cross SI, Sw (ft/ft)	= 0.083
Gutter Width (ft)	= 2.00
Invert Elev (ft)	= 6937.66
Slope (%)	= 7.00
N-Value	= 0.015

Calculations

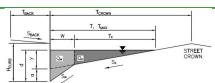
Compute by: Q vs Depth No. Increments = 50

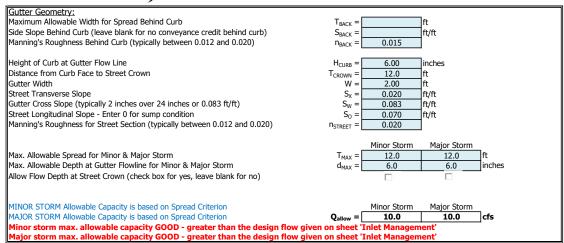
Highlighted		
Depth (ft)	=	0.16
Q (cfs)	=	0.889
Area (sqft)	=	0.15
Velocity (ft/s)	=	5.79
Wetted Perim (ft)	=	2.09
Crit Depth, Yc (ft)	=	0.26
Spread Width (ft)	=	1.92
EGL (ft)	=	0.68



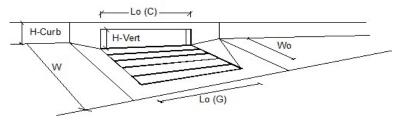
Reach (ft)

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Lot 1, The Knoll Development Rights Withdrawal and Resubdivision Plat Inlet ID: DP-1.b.1 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)



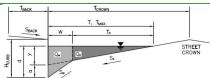


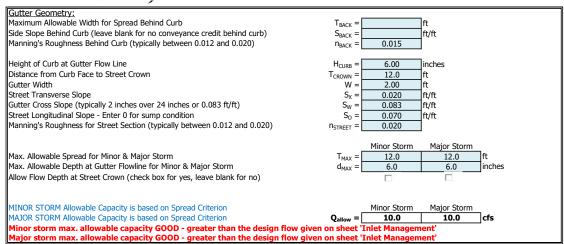
INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.01 (April 2021)



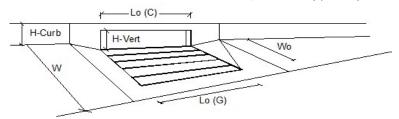
Design Information (Input) Denver No. 16 Combination		MINOR	MAJOR	
Type of Inlet	Type =	Denver No. 1	6 Combination	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	L _o =	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	1.73	1.73	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C_f - $G =$	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C_f - C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity'		MINOR	MAJOR	_
Total Inlet Interception Capacity	Q =	0.2	0.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b =$	0.0	0.1	cfs
Capture Percentage = Q _a /Q _o =	C% =	82	81	%

(Based on Regulated Criteria for Maximum Allowable Flow Depth and Spread) Project: Lot 1, The Knoll Development Rights Withdrawal and Resubdivision Plat Inlet ID: DP-1.b.2 ALLOWABLE CAPACITY FOR ONE-HALF OF STREET (Minor & Major Storm)





INLET ON A CONTINUOUS GRADE MHFD-Inlet, Version 5.01 (April 2021)



Design Information (Input) Denver No. 16 Combination		MINOR	MAJOR	_
Type of Inlet	Type =	Denver No. 1	6 Combination	
Local Depression (additional to continuous gutter depression 'a')	a _{LOCAL} =	2.0	2.0	inches
Total Number of Units in the Inlet (Grate or Curb Opening)	No =	1	1	
Length of a Single Unit Inlet (Grate or Curb Opening)	$L_o = [$	3.00	3.00	ft
Width of a Unit Grate (cannot be greater than W, Gutter Width)	$W_o =$	1.73	1.73	ft
Clogging Factor for a Single Unit Grate (typical min. value = 0.5)	C_f - $G = $	0.50	0.50	
Clogging Factor for a Single Unit Curb Opening (typical min. value = 0.1)	C_f - C =	0.10	0.10	
Street Hydraulics: OK - Q < Allowable Street Capacity		MINOR	MAJOR	
Total Inlet Interception Capacity	Q =	0.3	0.6	cfs
Total Inlet Carry-Over Flow (flow bypassing inlet)	$Q_b = $	0.1	0.2	cfs
Capture Percentage = Q _a /Q _o =	C% =	80	73	%



APPENDIX C

WATER QUALITY CALCULATIONS



CIVIL	ENGINEERS	1	SURVEYOR
CIVIL	ENGINEERS		SURVETUR

141 9th Street ~ P.O. Box 774943 Steamboat Springs, Colorado 80477 (970) 871-9494 www.LANDMARK-CO.com

DESIGNER: Matthew Eggen	
DATE: 10/5/2022	
POND ID:	

FAA Method Detention Estimate Per section 5.11.7.2 of the City of Steamboat Springs Drainage Criteria

$$V_i = (CiA)(T_c)(60 \text{ sec/min})$$
 (5.11.1)

Where:

 $V_r = \text{inflow volume (ft}^3)$

C = Rational Method runoff coefficient for the major or minor storm A = watershed area draining to the detention pond (acres)

 T_c = Rational Method time of concentration (min)

i = design rainfall intensity (in/hr)

$$V_a = (Allowable \, \text{Re} \, leaseRate)(T_c)(60 \, \text{sec/min})$$
 (5.11.2)

Where:

 $V_o = \text{outflow volume (ft}^3)$

 T_{ϵ} = Rational Method time of concentration (min)

Allowable release rate shall be determined per this Section (cfs).

A (acres) =	4.98
Tc (min) =	14.63

<-- INPUT from impervious calcs

<-- INPUT from Tc calcs

Minor Storm (5-Year)

Use Minor Storm for Detention only pond (No WQ)

•	
C ₅ =	0.35
i (in/hr) =	2.32
V_i (ft ³) =	
$Q_{A5} =$	
V_o (ft s) =	
$V_{req}(ft^3) =$	2005

<-- INPUT from impervious calcs

<-- INPUT from runoff calcs

<-- INPUT from historic runoff calcs

Major Storm (100-Year)

 $C_{100} 0.58$ i (in/hr) 5.06 V_i (ft³) 12,805 **Q**_{A100} 10.00 V_{o} (ft³) 8,777 $V_{req} (ft^3) | 4028$

<-- INPUT from impervious calcs

<-- INPUT from runoff calcs

<-- INPUT from historic runoff calcs



CIVIL ENGINEERS	I SURVEYORS
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141 9th Street ~ P.O. Box 774943 Steamboat Springs, Colorado 80477 (970) 871-9494 www.LANDMARK-CO.com

PROJECT:	2571-001
DESIGNER:	Matthew Eggen
DATE:	10/5/2022
POND ID:	

WQCV DESIGN CALCULATION - 12 HOUR DRAIN TIME Sand Filter or Bioretention (Rain Garden)			
REQUIRED STOR	AGE & SAND FILTER SIZE:		
	BASIN AREA (AC) = 4.98 < INPUT from impervious	us calcs	
ВА	SIN IMPERVIOUSNESS PERCENT = 39% < INPUT from impervious	us calcs	
	BASIN IMPERVIOUSNESS RATIO = 0.3907 < CALCULATED		
	d6 (in) = 0.34 < INPUT depth of avera	ge runoff producing storm	
	WQCV (watershed inches) = 0.11 < CALCULATED from N	MHFD Vol.3, Equation 3-1	
	$V(ft^3) = 2,433$ < CALCULATED from N	MHFD Vol.3, Equation 3-2	
SAND FILTER	17	JSCDM Vol.3, Equation SF-2	
BIORETENTION	A _f , Minimum Flat Filter Area (ft ²) = 1,695 < CALCULATED from L	JSCDM Vol.3, Equation B-2	
4" UNDERDRAIN	ORIFICE:		
	Pond Bottom Elev (ft) = < INPUT per grading pla	an	
	Underdrain invert at outlet (ft) = < INPUT per plan		
	Distance to center of orifice (ft) = 0.04 < CALCULATED	3/8" MIN. TO	
	Orifice Diameter (in) = 2.61 < CALCULATED	PREVENT	
OUTLET PIPE*:			
0012211112.		Typical Manning's n	
	Q ₁₀₀ (cfs) = 10.00 < INPUT from runoff cal		
	<u> </u>	Material n	
	120% * Q100 12.0 < CALCULATED	CMP 0.024	
	- 0.00 NIDUT	HDPE 0.020	
	n 0.02 < INPUT based on pipe	material RCP 0.012	
	S ₀ 0.02 ft/ ft < INPUT per plan		
	d ₁₀₀ (in) 19.53 in		

^{*} Calculate only if a stand alone waterquality pond (no detention)



APPENDIX D

With CDs

OWNERSHIP AND MAINTENANCE PLAN



APPENDIX E

CITY FORMS & CHECKLISTS

Standard Form No. 3 Final Drainage Study Checklist

Instructions:

- 1. The applicant shall identify with a "check mark" if information is provided with letter. If applicant believes information is not required, indicate with "N/A" and attach separate sheet with explanation.
- 2. The reviewer will determine if information labeled "N/A" is required and whether additional information must be submitted.

l.	Ge	ne	ral
	uc		ıaı

I. General	
X B. Report C. Drawir 36) inc	typed and legible in $8\frac{1}{2}$ " x 11" format. bound (comb, spiral, or staple – no notebook). In the large that are $8\frac{1}{2}$ x 11 or 11 x 17 bound within report, larger drawings (up to 24 x cluded in a pocket attached to the report. Drawings shall be at an appropriate size ale to be legible and include project area.
II. Cover	
X B. Project X C. Prepar	Type – Final Drainage Study. t Name, Subdivision, Original Date, Revision Date. er's name, firm, address, phone number. T" for 1 st submittal and revisions; "FINAL" once approved.
III. Title Sheet	
X C. Note: confor the acconfirm	of Contents. cation, PE Stamp, signature, and date from licensed Colorado PE. City of Steamboat Springs plan review and approval is only for general mance with City design criteria and the City code. The City is not responsible for curacy and adequacy of the design, dimensions, and elevations that shall be ned and correlated at the job site. The City of Steamboat Springs assumes no asibility for the completeness or accuracy of this document.
IV. Introduction	
	ption of site location, size in acres, existing and proposed land use, and any ent background info.

V. Drainage Criteria and Methodology Used

X	A. Identify design rainfall and storm frequency.
X	B. Identify the runoff calculation method used.
X	C. Identify culvert and storm sewer design methodology.
X	D. Identify detention discharge and storage methodology.
X	E. Discuss HEC-HMS methodologies and parameters, if HEC-HMS is used.

X B. Reference planning application type and plan set date and preparer.

X C. Identify drainage reports for adjacent development.

VI. Existing Conditions (Pre-Development/Historic) X A. Indicate ground cover, imperviousness, topography, and size of site (acres). X B. Describe existing stormwater system (sizes, materials, etc.). X C. Describe other notable features (canals, major utilities, etc.). X D. Note site outfall locations and ultimate outfall location (typically Yampa River). X E. Note capacity of existing system and identify any constraints. X F. Identify NRCS soil type. X G. Discuss any existing easements. X H. Identify the FEMA Map reviewed, if site is in floodplain/way, and zone designation. VII. Proposed Conditions X A. Indicate ground cover, imperviousness, topography, and disturbed area (acres). X B. Describe proposed stormwater system (sizes, materials, etc.). X C. Describe proposed outlets and indicate historic and proposed flow for each. X D. Include calculations for all culverts, ditches, ponds, etc. in appendix. X E. Include a summary table for the 5- and 100-year events showing historic flow and proposed flow for total site and each basin. X F. Discuss proposed easements. X G. Describe off-site flows to be passed thru site. X H. Summarize any impacts to downstream properties or indicate none. Reference CLOMR/LOMR and impacts. I. Detention Ponds. 1. Indicate pond volume and area (size and depth) requirement. 2. Indicate release rates. 3. Discuss outfall design, location, and overflow location. 4. Discuss maintenance requirements. J. Curb and Gutter 1. Indicate gutter capacity. 2. Indicate curb capacity. 3. Indicate design velocity 4. Indicate design depth of flow in street. K. Culverts 1. Indicate whether each culvert is under inlet or outlet control. 2. Show that headwater is less than the maximum allowable. With CDs 3. Indicate design velocity. 4. Indicate required and provided flow rates. 5. Discuss whether outlet protection is required and what will be used. L. Inlets 1. Indicate inlet capacity. 2. Indicate the type of inlet(s) used. M.Channels 1. Indicate design velocity (and type of dissipation if required). 2. Indicate required and provided flow capacity. With CDs

3. Show critical cross-section(s) including water surface.

N. Site Discharge

1. Discuss use and design of detention to ensure discharge is less than or equal to historic flow.

2. Provide documentation that downstream facilities are adequate and no adverse impacts to downstream property owners (i.e. no rise certification)

VIII. Post Construction Stormwater Management X A. Discuss in general terms which permanent BMP practices will be used to control pollutant and sediment discharge after construction is complete. Exhibit A, Storm Water Quality Plan shall be attached that will give details (see separate checklist)

IX

IX. Conclusions	
 X A. Provide general summary. X B. Note if site complies with criteria and any variances to criteria. X C. Indicate if peak proposed flow is less than, equal to, or greater than peak historic flor for each outfall, design point, and for the total site. X D. List proposed new stormwater system requirements. 	·W
 X. References X. A. Provide a reference list of all criteria, master plans, drainage reports and technical information used. 	
XI. Tables	
X A. Include a copy of all tables prepared for the study.	
XII. Figures	
 X A. Vicinity Map. X B. Site Plan (include the horizontal and vertical datum used and all benchmarks). 	

- - C. Existing conditions.
- 1. Delineate existing basin boundaries.
- 2. Delineate offsite basins impacting the site.
- 3. Show existing and proposed topography at an interval of at least 2-ft.
- 4. Show existing runoff flow arrows.
- 5. Show existing stormwater features (structures, sizes, materials, etc.).
- 6. Show floodplain limits and information.
- 7. For each basin show bubble with basin number, acreage and % impervious.
- 8. For each outlet show bubble with acreage and historic flow and proposed flow or provide information in summary table on figure.
 - D. Proposed Conditions
- 1. Delineate proposed basin boundaries.
- 2. Show proposed runoff flow arrows.
- 3. Show existing and proposed topography at an interval of at least 2-ft.
- 4. For each basin show bubble with basin number, acreage and percent impervious or provide a summary table or figure.
- 5. For each outlet show bubble with acreage, historic flow, and proposed flow or provide a summary table or figure.
- 6. Show floodplain limits and information.
- 7. Show proposed building footprints and FFE for commercial and multi-family
- 8. Show property lines and easements (existing and proposed).
- 9. Label public and private facilities. A general note can be placed on the plans in lieu of labeling all facilities, if applicable.

XIII. Appendices ____X___ A. Runoff Calculations. ____X___ B. Culvert Calculations. ____X___ C. Pond Calculations. ____X___ D. Other Calculations. Acknowledgements Standard Form No. 3 was prepared by: _____Matthew Eggen ______ 10/5/2022 Date Include Attachment A - Scope Approval Form (see Standard Form No. 5)

Include Attachment B - Storm Water Quality Plan (see Standard Form No. 4)

PROJECT SHEET – BASE DESIGN STANDARDS (Site is not constrained)

Complete a Project Sheet for each project that includes Permanent Stormwater Treatment Facilities.

SITE INFORMATION

Project Name:	Lot 1,	, The Knoll Development Rights Withdra	wal and Resubdivision Plat	
Project Location	on: Stea	imboat Springs, CO		
Submitted Dat	:e: 10	/5/2022	Submitted By: Landmark Consultants, Inc.	
Acreage Distu	rbed: 5.	94		
Existing Imper	vious: 26	6%	New Net Impervious: 39%	
Review Date:			Reviewed By:	
Preparer	City	Requirements		
w/ CD's		Design Details are included for all Treatr	ment Facilities	
		List or include a description of any source controls or other non-structural practices:		
	Select BMP based on expected pollutant type - snow storage Maintain existing drainage pattern			

DESIGN STANDARDS

Multiple Design Standards may be used on a site, as necessary, to meet the requirements, but only one Design Standard may be used for each treatment facility's tributary area. Evaluation of suitability of permanent stormwater treatment facilities is based on meeting the specified Design Standard and ease of long-term maintenance. Facilities must be designed in accordance with the most current versions of the City's Engineering Standards and Volume 3 of the USDCM and meet the specific requirements for each Design Standard used.

- 1. Indicate below, which Design Standard(s) will be used for the project, and
- 2. Complete a separate, corresponding Design Standards checklist for each facility (e.g., WQCV)

Design Standard	Quantity	Tributary Area	Location/Identifying information
WQCV	2,433-ft3	4.98-acres	D1.b
Pollutant Removal			
Runoff Reduction			

Standard Form No. 4 Stormwater Quality Plan Checklist

This list is not an exhaustive list of every possible item that may be required or requested in a Stormwater Quality Plan but provides a general guideline for preparation of the Stormwater Quality Plan.

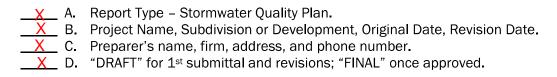
Instructions:

- 1. The applicant shall identify with a "check mark" if information is provided within the Stormwater Quality Plan. If applicant believes information is not required, indicate with "N/A" and attach separate sheet with explanation. If information is included with the associated drainage letter or study, indicated with a "D."
- 2. The reviewer will determine if information labeled "N/A" is required and whether additional information must be submitted.

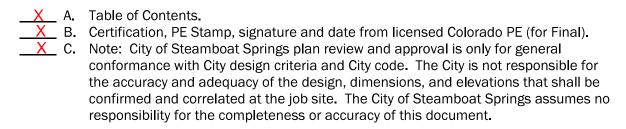
I. General

<u>X</u> A.	Report typed and legible in $8\frac{1}{2}$ " x 11" format.
<u> </u>	Report bound (comb, spiral, or staple – no notebook) and in digital PDF format.
<u> </u>	Drawings that are 11" x 17" bound within letter, larger drawings (up to 24" x 36")
	included in a pocket attached to the letter, and a digital PDF copy. Drawings shall be
	at an appropriate size and scale to be legible and include project area.

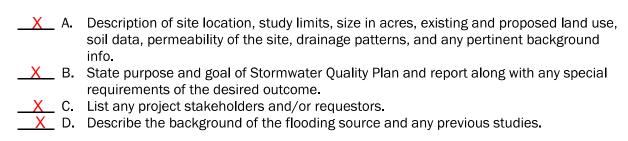
II. Cover



III. Title Sheet



IV. Introduction and Background



V. Desig	n Cr	iteria and Methodology Used		
X	Α.	Identify design rainfall and storm frequency used to design permanent stormwater		
X	В	treatment facilities. Identify the runoff calculation method used to design permanent stormwater		
X	C.			
X	D.	which it will use to meet the standard. Provide all details supporting the use of the selected design standard.		
VI. Prop	osec	d Conditions		
X	Α.	Identify total site area, total site imperviousness, area to be treated, and impervious		
X	В.	area to be treated. Include justification for treating less than the total site area. Describe potential site contaminant sources including sediment.		
<u>X</u>	C.	Identify source and quantity of on-site and off-site stormwater flows that need to be managed and how they will be managed.		
X	D.	For each permanent treatment facility, identify the design standard, MDCIA level (if applicable), area treated (& percentage of total), imperviousness of area treated, C values of area treated, soil types, and all pertinent data for design.		
<u>X</u>	Ε.	Volume based facilities: Provide total storage pond volume, WQCV, drain time, release rate, sediment storage, outlet & overflow structures, area and depth of pond,		
X	F.	micropool, forebays, etc. (include all calculations in the appendix). Flow based facilities: Provide design flow rate and all treatment calculations and how flows larger than the water quality design flow rate will be handled. If proprietary facilities are proposed, provide the justification and sizing requirements from		
<u>X</u>	G.	manufacturer. If stormwater detention is provided, discuss how water quality is provided within the detention facility. No underground detention is allowed.		
VII. Ope	ratio	n and Maintenance Plan Requirements		
See tem	plat	te 0&M plan and guidance document. TO BE SUBMITTED WITH CD's		
	Α.	Describe general project information, facility description, ROW and access information, vegetation management, hydraulic design parameters, environmental permitting, snow and ice control, and additional pertinent information in the notes.		
	В.	Indicate, describe, and detail the permanent stormwater treatment facilities.		
	E.	treatment facilities and who is responsible for them. Identify design specifications for construction.		
Acknowle				
Standard	For	m No. 4 prepared by: Matthew Eggen 10/5/2022 Date		

Include appropriate Project Sheet(s) and Design Checklist(s) (See Section 5.12) Include this form as part of the Stormwater Quality Plan.

Standard Form No. 5 Drainage and Stormwater Treatment Scope Approval Form

Prior to starting a development plan and before the first drainage submittal, a Drainage and Stormwater Treatment Scope Approval Form must be submitted for review and signed by the City Engineer. A signed form shall also be included in every drainage submittal as Attachment A. This Scope Approval Form is for City requirements only. Values may be approximate. The City encourages supporting calculations and figures to be attached.

Project Information			
Project name:	Lot 1, The Knoll Development Rights Withdrawal and Resubdivision Plat		
Project location:	Steamboat Grand Resort Hotel		
Developer name/contact info:	Steamboat Resort Development 3501 Wazee Street, Denver CO		
Drainage engineer name/contact info:	Landmark Consultants, Inc. matte@landmark-co.com (970) 819-9494		
Application Type:	Preliminary Plat		
Proposed Land Use:	Resort Residential		
Project Site Parameters	S		
Total parcel area (acres	s):	13.9	
Disturbed area (acres):		4.34	
Existing impervious are applicable):	ea (acres, if	0.38	
Proposed new impervious	ous area (acres):	1.96	
Proposed total impervious	ous area (acres):	2.06	
Proposed number of pr	roject outfalls:	2	
Number of additional parking spaces:		0	
Description and site percentage of existing cover/land use(s):		13.52 acres - Open space, pervious area 0.38 acres - Asphalt Trail, pavements, building	
Description and site percentage of proposed cover/land use(s):		0.68 acres - Pavements 1.28 acres - ~70% impervious development of proposed lot 1	
Expected maximum proposed conveyance gradient (%):		38%	
Description of size (acres) and cover/land use(s) of offsite areas draining to the site		NA	

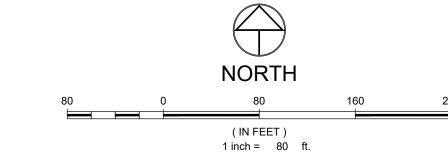
Type of Study Required: Drainage Letter Final Drainage Study	☐ Conceptual Drainage StudyX Stormwater Quality Plan		
Hydrologic Evaluation: X Rational Method CUHP/SWMM	HEC-HMS Other		
Project Drainage			
Number of subbasins to be evaluated:	2		
Presence of pass through flow (circle):	YES NO		
Description of proposed stormwater conveyance on site:	storm water will generally be collected in swales and pipes on the west side of the parcel and conveyed to the on-site WQ/Detention basin. Storm water on the east side of the parcel will not convey additional flows and therefore be left as is.		
Project includes roadway conveyance as part of design evaluation (circle):	YES NO		
Description of conveyance of site runoff downstream of site, identify any infrastructure noted in Stormwater Master Plan noted as lacking capacity for minor or major storm event:	The western site stormwater will leave the site at an existing culvert under Mount Werner Circle which outfalls into Wildhorse Meadows. The outfall pipe is not listed as a "Problem or Need" in the Citywide Stormwater Plan.		
Detention expected onsite (circle):	YES NO		
Presence of Floodway or Floodplain on site (circle):	YES NO		
Anticipated modification of Floodway or Floodplain proposed (circle):	YES NO		
Describe culvert or storm sewer conveyance evaluative method:	HY-8, Autodesk Storm and Sanitary Sewer Analysis		
Permanent Stormwater Treatment Facility D standard per tributary basin):	esign Standard (check all that apply with only one		
■ WQCV Standard	☐ Infiltration Standard		
Constrained Redevelopment WQCV Stand	dard		
Constrained Redevelopment TSS Standa	rd		
Constrained Redevelopment Infiltration S	Standard		

Project Permanent Stormwater Treatment	
Justification of choice of proposed design standard, including how the site meets the constrained redevelopment standard, infiltration test results, etc.:	Proposed improvements require detention to maintain historic discharge rates and water quality treatment due to increased impervious surface area.
Concept-level permanent stormwater treatment facility design details (type, location of facilities, proprietary structure selection, treatment train concept, etc.):	One bioretention basin will treat the WQCV and also provide adequate detention for the 5-year and 100-year storms.
Proposed LID measures to reduce runoff volume:	One bioretention basin will treat the WQCV and also provide adequate detention for the 5-year and 100-year storms.
Will treatment evaluation include off-site, pass through flow (circle):	YES NO

Approvals

Matthew Eggen, Landmark Consultants, Inc.	. 9/21/22	(970)819-8893
Prepared By: (Insert drainage engineer name & firm)	Date	Phone number
Approved By:		APPROVED
Printed Name: City Engineer	Date	to be generally in accordance with CITY ENGINEERING STANDARDS
		10/04/2022





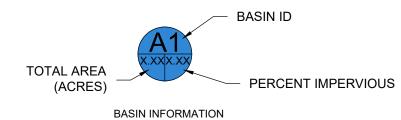
LEGEND:

EXISTING STORM SEWER PROPOSED STORM SEWER PROPOSED STORM INLET (CURB & AREA) PROPOSED MAJOR CONTOUR PROPOSED MINOR CONTOUR EXISTING MAJOR CONTOUR EXISTING MINOR CONTOUR PROPOSED SWALE PROPOSED CURB & GUTTER PROPERTY BOUNDARY PROPOSED LOT LINE EXISTING RIGHT OF WAY FLOOD HAZARD LIMITS

PROPOSED SPOT ELEVATION

PROPOSED OVERLAND FLOW DIRECTION W/SLOPE PROPOSED CHANNELIZED FLOW DIRECTION W/ SLOPE

EXISTING CHANNELIZED FLOW DIRECTION



NOTES:

- THE SIZE, TYPE AND LOCATION OF ALL KNOWN UNDERGROUND UTILITIES ARE APPROXIMATE WHEN SHOWN ON THESE DRAWINGS. IT SHALL BE THE RESPONSIBILITY OF THE DEVELOPER TO VERIFY THE EXISTENCE OF ALL UNDERGROUND UTILITIES IN THE AREA OF THE WORK. BEFORE COMMENCING NEW CONSTRUCTION, THE CONTRACTOR SHALL BE RESPONSIBLE FOR LOCATING ALL UNDERGROUND UTILITIES AND SHALL BE RESPONSIBLE FOR FOR ALL UNKNOWN UNDERGROUND UTILITIES.
- ALL PROJECT DATA IS ON VERTICAL DATUM; NAVD 88. SEE NOTES SHEET FOR BENCHMARK REFERENCES.
- ELEVATIONS FOR IMPROVEMENTS THAT ARE CONTROLLED BY ADJACENT EXISTING FACILITIES (SUCH AS PROPOSED GUTTERS ALONG EXISTING ASPHALT) MAY REQUIRE ADJUSTMENT BASED ON ACTUAL CONDITIONS. COORDINATE WITH ENGINEER TO ENSURE A CONSISTENT SECTION WITH SMOOTH TRANSITIONS WHERE NECESSARY.
- 4. SEE SOILS REPORT FOR PAVEMENT, SUBGRADE AND MATERIAL PREPARATION, DESIGN AND RECOMMENDATIONS.
- 5. ALL CURB SPOTS SHOWN ARE FLOWLINE ELEVATIONS, UNLESS NOTED OTHERWISE. ALL OTHER SPOTS ARE FINISHED GRADE ELEVATIONS.

	<u> </u>	Table 1:	Basin Hy	drology Sun	nmary		
Basin	Total Area (acres)	%lmp	C ₅	C ₁₀₀	T _c (min)	Q₅ (cfs)	Q ₁₀₀ (cfs)
H1	7.93	26%	0.28	0.56	15.03	5.08	22.05
H2	4.15	40%	0.35	0.58	16.54	3.09	11.23
D1.a	4.52	41%	0.35	0.58	17.24	3.35	12.05
D1.b	4.98	39%	0.35	0.58	14.63	4.02	14.58
DP-1.b.1	0.16	62%	0.47	0.64	9.37	0.23	0.69
DP-1.b.2	0.11	100%	0.90	0.96	7.45	0.34	0.78
D2	3.88	44%	0.37	0.59	16.54	3.06	10.70
Allowa	able Outflow	for Detent	ion Calcu	lation			
Design Storm Q _H		Q _{UD}	$\mathbf{Q}_{\mathtt{A}}$	Q _H	Historic peak flow (cfs)		
5-Year 5.		5.08	3.35	1.73	Q _{UD}	Undetained flow (cfs)	
100-Year		22.05	12.05	10.00	Q_A	Allowable peak flow from	
						detention facility (cfs)	
		i	3ioretent	ion Pond Su	mmary		
Basin	Sand Filter Flat Area (ft²)		WQCV ¹ (ft ³)	Detention ² V ₅ (ft ³)	Detention ² V ₁₀₀ (ft ³)	V ₁₀₀ + WQCV (ft ³)	Total Volum (ft ³)
	Required	Provided	Required			Provided	
WQ-1	1059	1,113	2,433	2,005	4,028	6,461	6,481
			Total Treated Area (acres)				4.98

Total Disturbed area (acres) Percent Treated (%)

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— — — — 6805 – — — — —

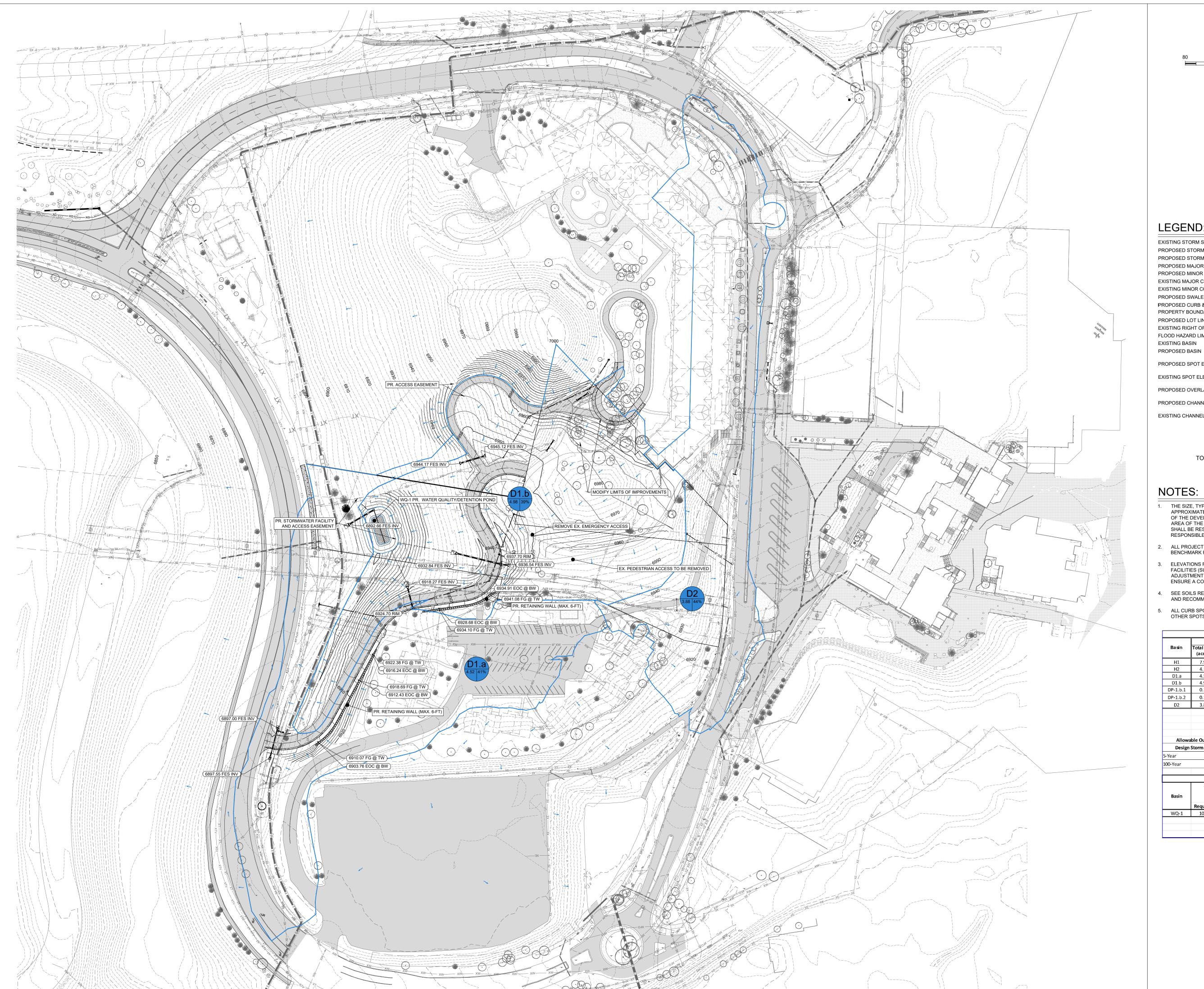
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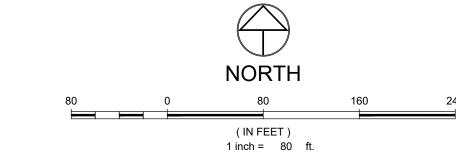
2.0%

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5.94

SHEET FIG 2





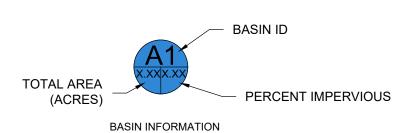
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EXISTING CHANNELIZED FLOW DIRECTION



00.10

00.10 X

2.0%

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Percent Treated (%)

FIG 3